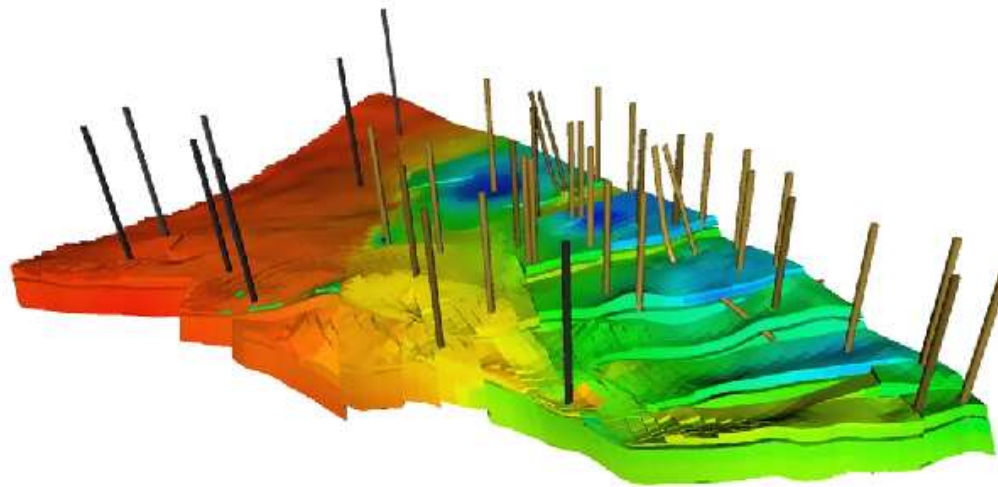


# Determining Identifiable Parameterizations for Large-scale Physical Models in Reservoir Engineering



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# Outline

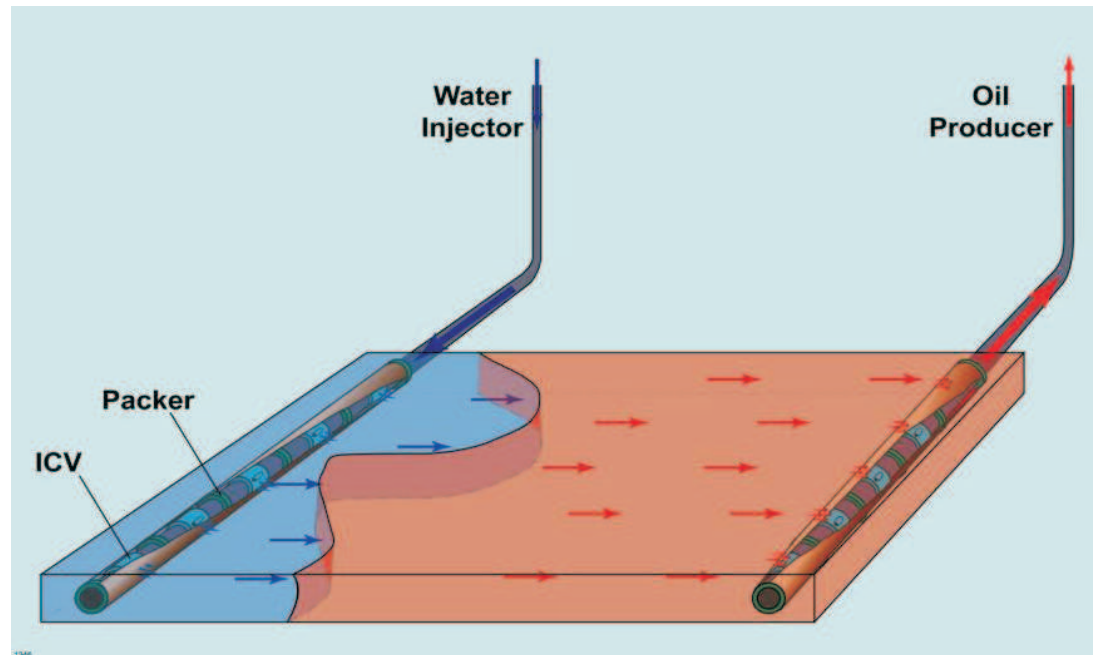
- Reservoir engineering and parameter estimation
- Structural identifiability
- Determining identifiable parameterizations
- Example with grid block permeability
- Summary

# Upstream oil industry - characteristics

- **Capital intensive:** well:  $1 - 100 * 10^6$  US\$, field:  $0.1 - 10 * 10^9$  US\$.
- **Uncertainty:** geology, oil price, limited data.
- Reservoir can only be **produced once**.
- Time scales stretch from days to **decades**.
- **Trends**
  - Produce more from existing reservoirs
  - Increasing knowledge- and data intensity
  - Move to model-based control

# Water flooding

- Inject water to push oil to producers.
- Increase oil recovery by manipulating ICVs in wells.
- Major influence of [permeability](#) on saturation behavior.



# Model equations

Model describes flow of water and oil through porous medium.

$$\begin{aligned}\frac{\partial}{\partial t} (\phi \rho_o [1 - S_w]) &= \nabla \cdot \left( \bar{k} \frac{k_{ro}}{\mu_o} \rho_o \nabla p \right) + q_o \\ \frac{\partial}{\partial t} (\phi \rho_w S_w) &= \nabla \cdot \left( \bar{k} \frac{k_{rw}}{\mu_w} \rho_w \nabla p \right) + q_w\end{aligned}$$

Discretization in space (grid blocks) and time gives nonlinear state-space model:

$$\begin{bmatrix} \mathbf{p}(k+1) \\ \mathbf{S}_w(k+1) \end{bmatrix} = \begin{bmatrix} \mathbf{A}_{11}(\mathbf{p}(k), \mathbf{S}_w(k)) & 0 \\ \mathbf{A}_{21}(\mathbf{p}(k), \mathbf{S}_w(k)) & 0 \end{bmatrix} \begin{bmatrix} \mathbf{p}(k) \\ \mathbf{S}_w(k) \end{bmatrix} + \begin{bmatrix} \mathbf{B}_1(\mathbf{p}(k), \mathbf{S}_w(k)) \\ \mathbf{B}_2(\mathbf{p}(k), \mathbf{S}_w(k)) \end{bmatrix} \mathbf{u}(k)$$

- $\bar{k}$  permeabilities in EACH grid block.
- Commonly  $10^5 - 10^6$  grid blocks!

# Reservoir simulation

- $\mathbf{u} \in \mathbb{R}^m$ : injection rates, pressures in producer wells.
- $\mathbf{y} \in \mathbb{R}^p$ : pressures in injector wells, production rates.

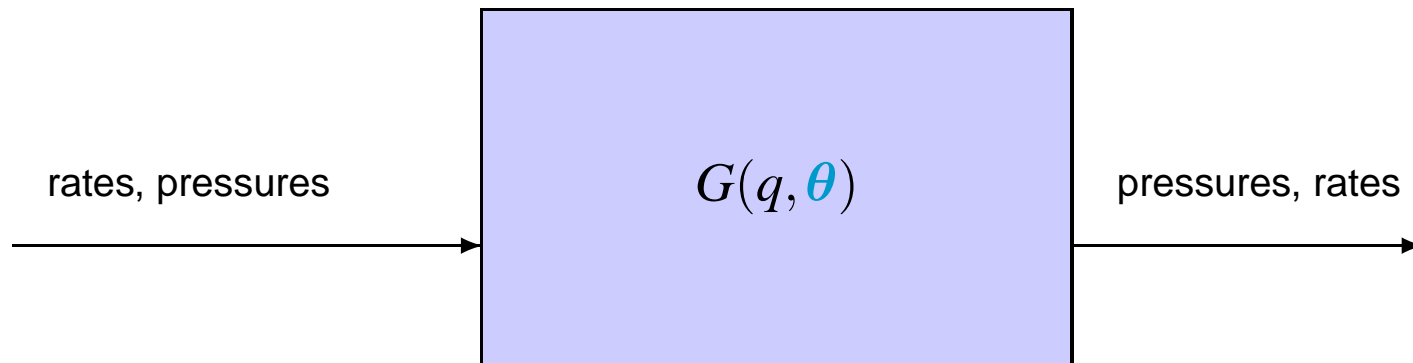
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# Parameter estimation

- Physical parameters (permeabilities) estimated from production measurements with e.g. RLS, EKF or EnKF.
- Challenges:
  - Many grid block permeabilities to be estimated ( $10^5 - 10^6$ ).
  - Limited number of wells.
- Option:
  - Determine identifiable subspace of parameter domain.
  - This leads to a map  $\bar{\mathbf{k}} = \mathbf{T}\boldsymbol{\rho}$ , where  $\dim \boldsymbol{\rho} \ll \dim \bar{\mathbf{k}}$ .
- Tool: Structural identifiability analysis.

# Structural identifiability

- First stated by Bellman and Åström (1970).
- Model is structurally identifiable if its physical **parameters** can be uniquely determined from the input-output behavior.



$$\mathbf{x}(k+1) = \mathbf{A}(\boldsymbol{\theta})\mathbf{x}(k) + \mathbf{B}(\boldsymbol{\theta})\mathbf{u}(k)$$

$$\mathbf{y}(k) = \mathbf{C}(\boldsymbol{\theta})\mathbf{x}(k) + \mathbf{D}(\boldsymbol{\theta})\mathbf{u}(k)$$

# Local structural identifiability

- The model structure is locally structurally identifiable from the input-output behavior at  $\theta^*$  if, for every  $\theta_1, \theta_2$  in the neighborhood of  $\theta^*$ ,  $G(q, \theta_1) = G(q, \theta_2) \rightarrow \theta_1 = \theta_2$ .
- $G(q, \theta) = \sum_{k=1}^{\infty} \mathbf{M}(k, \theta) q^{-k}$ , where  $\mathbf{M}(k) := \mathbf{C}(\theta) \mathbf{A}(\theta)^{k-1} \mathbf{B}(\theta)$
- Gather Markov parameters in

$$\vec{\mathbf{S}}_r(\theta) := [ \vec{\mathbf{M}}(1, \theta) \quad \vec{\mathbf{M}}(2, \theta) \quad \dots \quad \vec{\mathbf{M}}(r, \theta) ] \in \mathbb{R}^{1 \times pmr}.$$

- If  $\frac{\partial \vec{\mathbf{S}}_r(\theta)}{\partial \theta}$  has constant rank  $l$  in a neighborhood of  $\theta^*$ , then  $\vec{\mathbf{S}}_r(\theta)$  is locally injective at  $\theta^*$  if and only if  $l = q$ .

# Local structural identifiability

- Test local structural identifiability by rank test on

$$I_r := \left. \frac{\partial \vec{\mathbf{S}}_r}{\partial \boldsymbol{\theta}} \frac{\partial \vec{\mathbf{S}}_r^T}{\partial \boldsymbol{\theta}^T} \right|_{\boldsymbol{\theta}^*} = \sum_{i=1}^r \sum_{j=1}^p \left( \frac{\partial \mathbf{M}_{j^*}(i)}{\partial \boldsymbol{\theta}} \frac{\partial \mathbf{M}_{j^*}^T(i)}{\partial \boldsymbol{\theta}^T} \right) \Big|_{\boldsymbol{\theta}^*} \in q \times q.$$

where

$$\begin{aligned} \frac{\partial \mathbf{M}_{j^*}(k, \boldsymbol{\theta})}{\partial \boldsymbol{\theta}} &= \frac{\partial \mathbf{C}_{j^*}}{\partial \boldsymbol{\theta}} \mathbf{A}^{k-1} \mathbf{B} + \left( \mathbf{I}_q \otimes \mathbf{C}_{j^*} \mathbf{A}^{k-1} \right) \frac{\partial \mathbf{B}}{\partial \boldsymbol{\theta}} \\ &\quad + \sum_{l=1}^{k-1} \left( \mathbf{I}_q \otimes \mathbf{C}_{j^*} \mathbf{A}^{l-1} \right) \frac{\partial \mathbf{A}}{\partial \boldsymbol{\theta}} \mathbf{A}^{k-1-l} \mathbf{B}. \end{aligned}$$

- For a given model, the expression can be calculated exactly.
- Limitation: only local linearized situation can be handled.

# Observability and controllability

- $I_r$  can be expressed in terms of observability and controllability
- Recall  $I_r := \frac{\partial \vec{\mathbf{S}}_r}{\partial \boldsymbol{\theta}} \frac{\partial \vec{\mathbf{S}}_r^T}{\partial \boldsymbol{\theta}^T} \Big|_{\boldsymbol{\theta}^*}$
- Consider  $\frac{\partial \mathbf{B}}{\partial \boldsymbol{\theta}}$  and  $\frac{\partial \mathbf{C}}{\partial \boldsymbol{\theta}}$  zero, and  $q = 1$ ,  $p = 1$  and  $r = 4$ .
- Then  $\frac{\partial \vec{\mathbf{S}}_4}{\partial \boldsymbol{\theta}} = \begin{bmatrix} 0 & \mathbf{X} \end{bmatrix}$ , where

$$\mathbf{X} = \begin{bmatrix} \mathbf{C} & \mathbf{CA} & \mathbf{CA}^2 \end{bmatrix} \begin{bmatrix} \frac{\partial \mathbf{A}}{\partial \boldsymbol{\theta}} & & \\ & \frac{\partial \mathbf{A}}{\partial \boldsymbol{\theta}} & \\ & & \frac{\partial \mathbf{A}}{\partial \boldsymbol{\theta}} \end{bmatrix} \begin{bmatrix} \mathbf{B} & \mathbf{AB} & \mathbf{A}^2\mathbf{B} \\ & \mathbf{B} & \mathbf{AB} \\ & & \mathbf{B} \end{bmatrix}.$$

# Identifiable parameterization

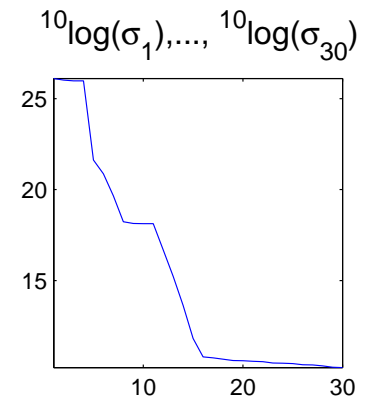
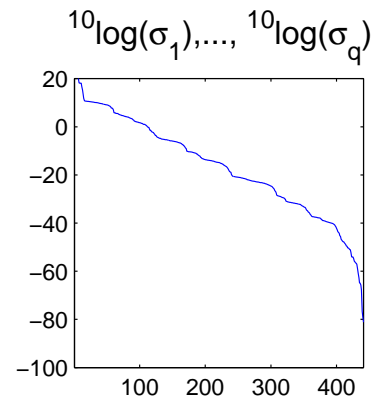
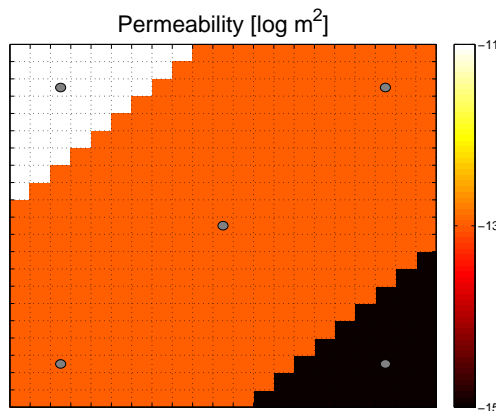
- Calculate  $I_r$  using  $\mathbf{A}$ ,  $\mathbf{B}$ ,  $\mathbf{C}$ , and their analytical derivatives to  $\theta$
- Use singular value decomposition (SVD) on  $I_r$

$$I_r = \begin{bmatrix} \mathbf{U}_1 \\ \mathbf{U}_2 \end{bmatrix}^T \begin{bmatrix} \Sigma_1 & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \mathbf{V}_1^T \\ \mathbf{V}_2^T \end{bmatrix},$$

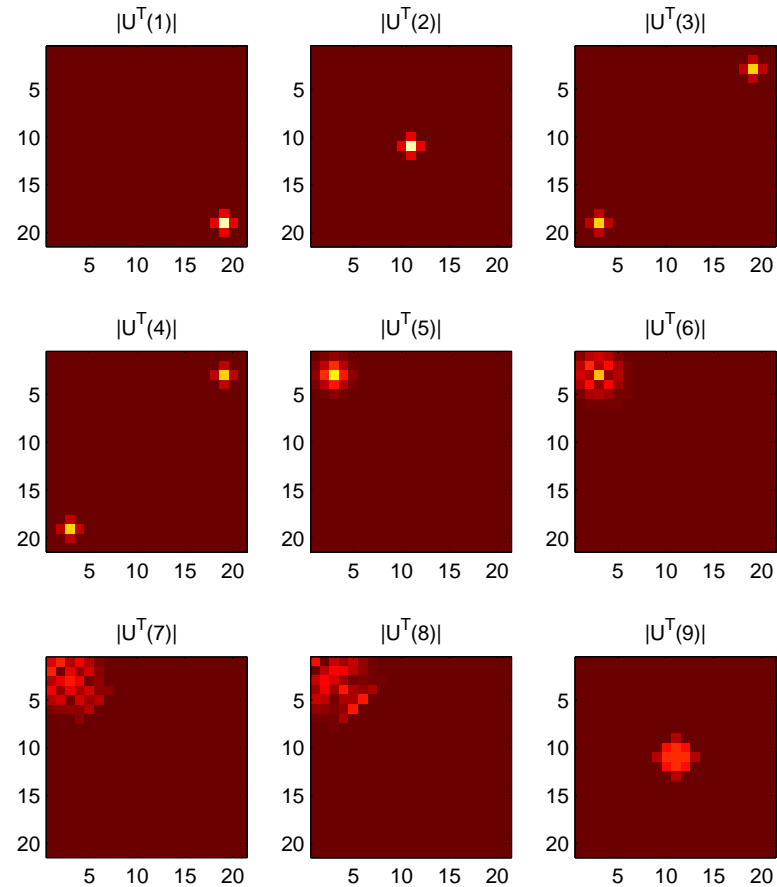
- Columns of  $\mathbf{U}_1$  are structurally identifiable directions in parameter space.
- Columns of  $\mathbf{U}_2$  are structurally *not* identifiable.
- Visualize each column vector (length  $q$ ) by projection onto reservoir grid ( $q$  grid blocks).

# Example

- Single-phase reservoir model with  $21 \times 21$  grid blocks.
- 5 wells (5 inputs, 5 outputs) measuring BHP and total well flow rate.
- Determine identifiable parameterization of permeability  $\bar{\mathbf{k}} \in \mathbb{R}^{441}$ .



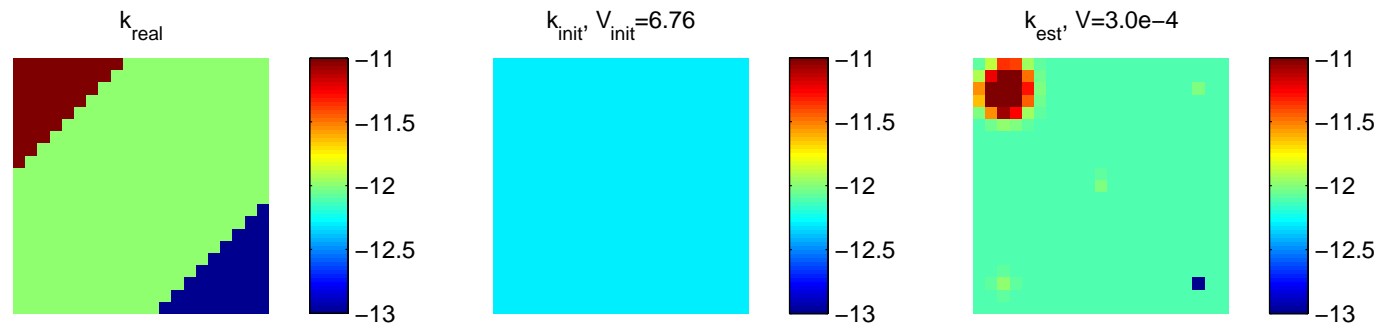
# Identifiable parameterization



First 9 column vectors of  $|U_1|$  projected on reservoir simulation grid.

# Estimation

- Use  $U_1$  to go from high-dimensional  $\bar{\mathbf{k}}$  to low-dimensional  $\alpha$ .
- Reparameterize permeability as  $\bar{\mathbf{k}} = \mathbf{U}_1 \alpha$ .
- Iteratively estimate  $\rho = \arg \min_{\rho} V(\mathbf{U}_1 \rho)$ .
- Advantage: only those (combinations of) grid block permeabilities are estimated that are relevant for the input-output behavior.



# Conclusions

- Developed analytical expression to test structural identifiability.
- Can be expressed in observability, sensitivity and controllability matrix.
- Determined with SVD most identifiable parameterization with strongly reduced number of parameters.
- Used parameterization to estimate permeability in reservoir model.