

Model Based Control and Optimization Challenges in Reservoir Engineering

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Delft University of Technology



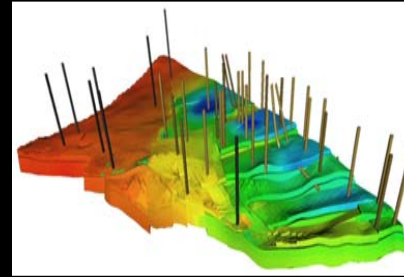
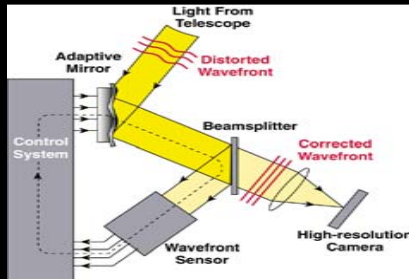
Oldest and largest of 3
Technical Universities in the
Netherlands:
Delft – Eindhoven - Twente

Founded in 1842 as an
engineering school

Now: 5000 employees, of which
2700 scientists, 15,000 students,
distributed over 8 engineering
faculties:

- Electrical, Math, Comp. Science
- Aerospace Engineering
- Applied Sciences
- Mechanical, Maritime, Mat. Eng.
- Civil Engin., Earth Sciences
- Industrial Design
- Techn. Policy Making and Manag
- Architecture

Delft Center for Systems and Control



University wide center and department within Mechanical Engineering

- 14 scientific (tenured) staff
- 40 PhD students
- 15 Postdocs
- 40 MSc students / year
- BSc programs ME, EE, AP,
- MSC programs ME, EE, AP
- 3TU MSc Systems and Control
- PhD programme DISC



Delft Center for Systems and Control

- Robert Babuska
- Bart De Schutter
- Paul Van den Hof
- Michel Verhaegen
- Okko Bosgra
- Alessandro Abate
- Xavier Bombois
- Arjan den Dekker
- Peter Heuberger
- Adrie Huesman
- Tamas Keviczky
- Gabriel Lopes
- Roland Tóth
- Ton van den Boom
- Jan Willem van Wingerden

Fundamentals:

- Modelling, control and optimization of complex, non-linear and hybrid systems
- Signal analysis, signal processing and data-based modelling (identification for control)

Mechatronics and Microsystems:



- Automotive systems
- Microfactory
- AFM nano-positioning
- Smart optics systems
- Electron microscopes
- Robotics

Traffic and Transportation:



- Discrete event and hybrid systems
- Distributed multi-agent systems
- Optimal adaptive traffic control
- Advanced driver assistance systems

Sustainable Industrial Processes:



- Increase of scale in process operation
- More flexibility in operation
- Economic optimization under operating constraints
- Process intensification
- Towards model-based process management
- hydrocarbon reservoir optimization; crystallization

Areas of interest

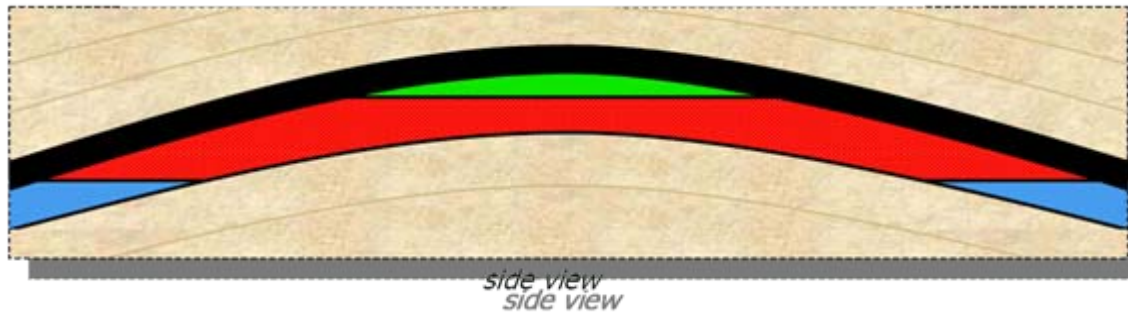
- System identification (LPV, experim.design, closed-loop, distributed)
- Autonomous model maintenance and monitoring in process control
- Nonlinear model-based control and economic optimization
- Parameter estimation in (large scale) physical structures
- Model-based measurement and control in electron microscopy

Applications

- Water flooding in reservoir engineering
- Crystallization processes
- Industrial hydrocarbon/gas-to-liquid production processes
- Intensified reaction systems (process intensification)
- Multiphase-flow systems (ILS)
- Microscopy (AFM, electron microscopes)

Oil Production

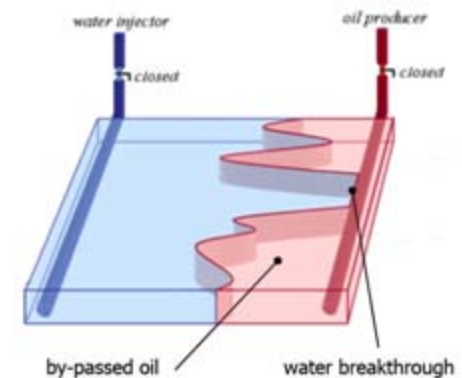
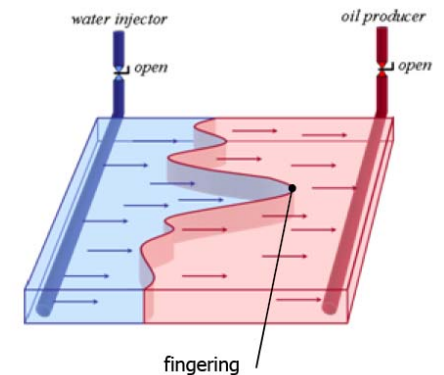
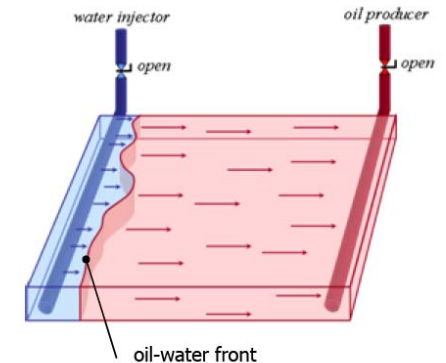
- Production from Oil Reservoirs
 - Porous rock with oil in pores
 - Geological structure heterogeneous
 - Very different rock properties within reservoir
 - $10^1 - 10^4$ km² in size
 - 10^2 m – 10^4 m underground
 - Difficult locations



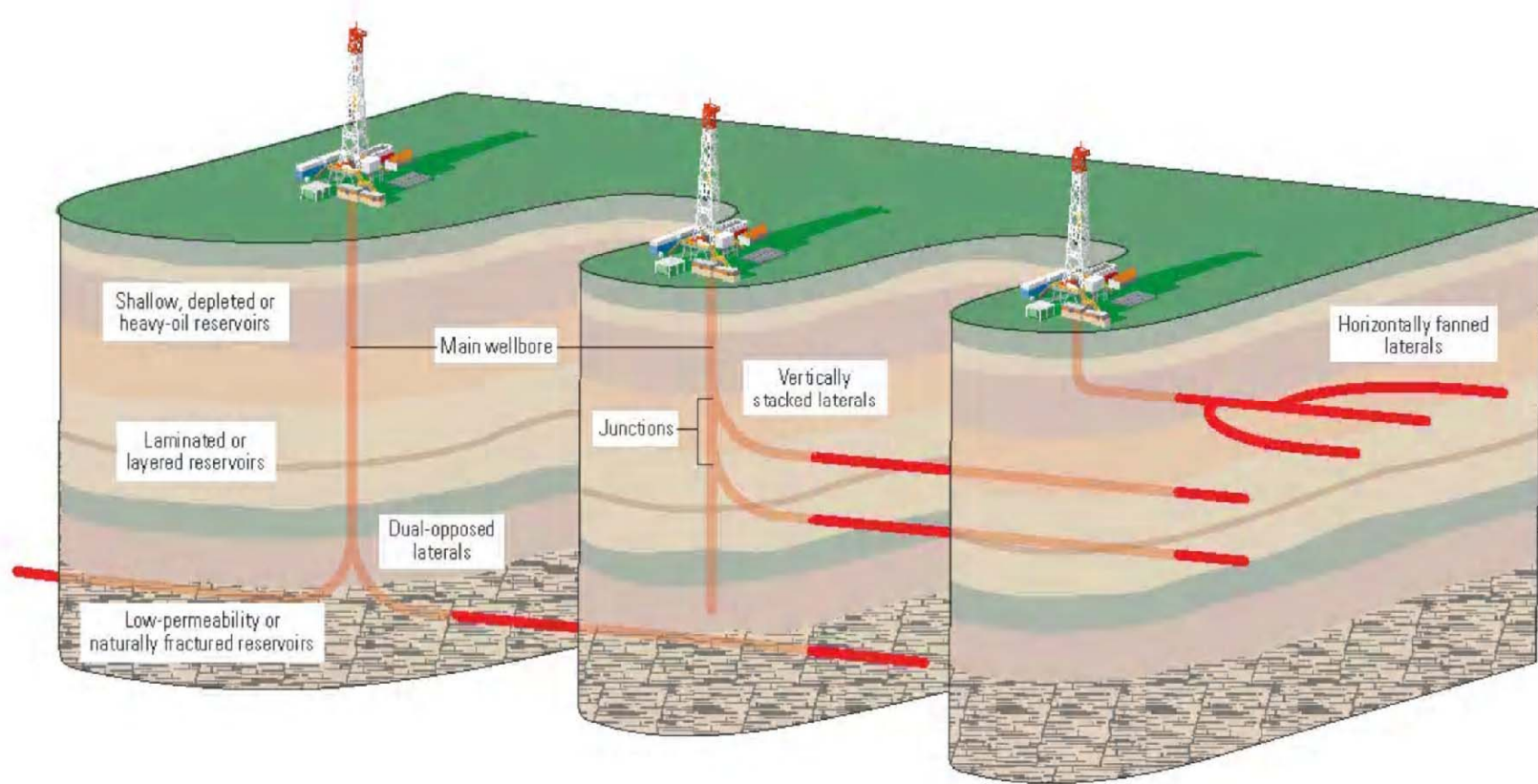
- cap rock
- water bearing reservoir rock
- non- reservoir rock
- oil bearing reservoir rock
- gas bearing reservoir rock

Oil Production

- Oil Production goes through multiple stages
 - Primary production
 - Secondary production
 - Tertiary production
- **Waterflooding** (WF) popular secondary production process
 - Reservoir pressure support
 - Sweeping the reservoir
- Essentially a batch process
 - Duration in the order of decades
 - On average **35%** of the oil is recovered



Smart well with inflow control valves



Main question to explore:

Can model-based control be of use in this field, to support the decision-making and operational strategies of the operators / field-managers ?

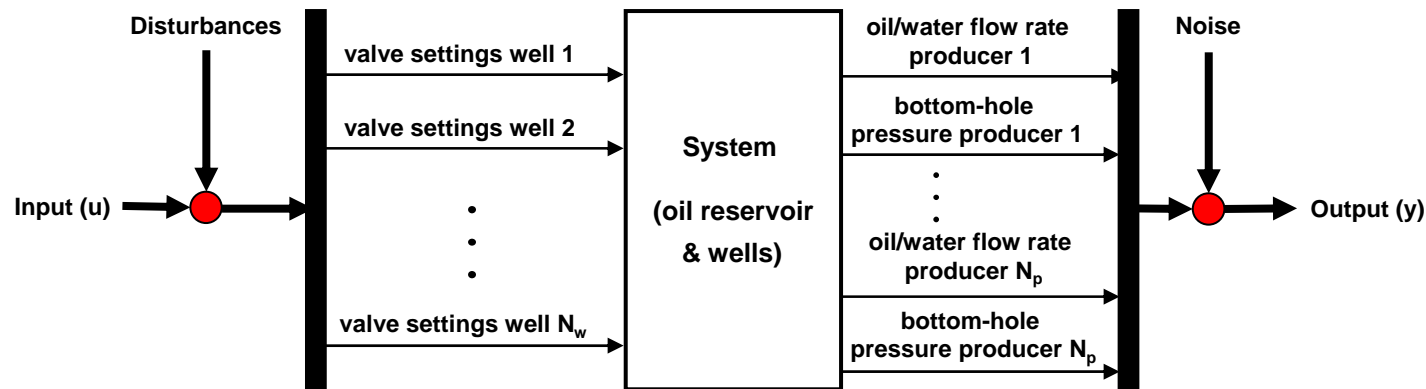
Contents

- Introduction – reservoir management
- **Dynamic model and control objectives**
- Optimal control example
- On-line estimation and control (closed-loop)
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- Additional optimization opportunities
- Discussion

The Models

System involves the reservoir, wells and sometimes surface facilities

- **Inputs:** control valve settings of the wells (injectors and producers)
 - Smart wells: multiple (subsurface) valves
- **Outputs:** (fractional) flow rates and/or bottomhole pressures
 - Smart wells: multiple (subsurface) measurement devices



Governing differential equations

isothermal two-phase (oil-water) flow

Mass balance:

$$\nabla(\rho_i u_i) + \frac{\partial}{\partial t}(\phi \rho_i S_i) = 0 \quad i = \{o, w\}$$

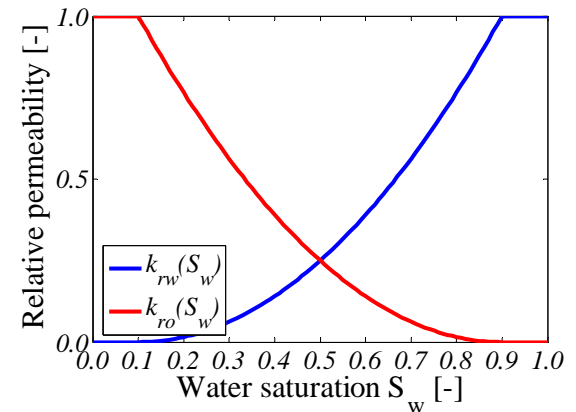
Momentum (Darcy's law):

$$u_i = -k \frac{k_{ri}}{\mu_i} \nabla p_i \quad i = \{o, w\}$$

Variables: p_o, p_w, S_o, S_w

Saturations satisfy: $S_o + S_w = 1$

Simplifying assumptions, a.o.: $p_o = p_w$



Discretization in space and time

State space model:

$$\begin{aligned} V(x_t)\dot{x}_t &= T(x_t)x_t + q_t; & x_0 \\ y_t &= h(x_t) \end{aligned}$$

$$\begin{aligned} y^T &= [p_{well}^T \quad q_{well,o}^T \quad q_{well,w}^T] \\ x^T &= [p_o^T \quad S_w^T] \end{aligned}$$

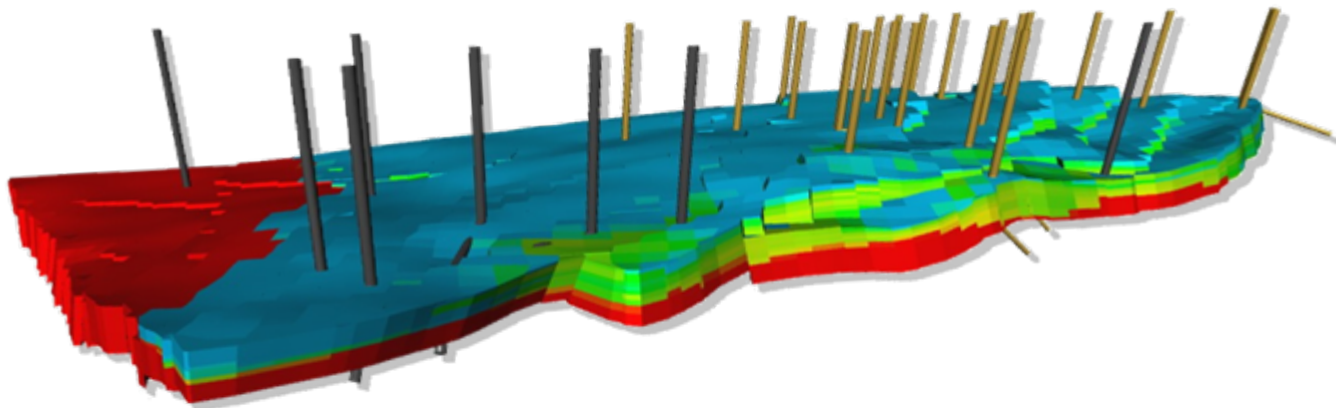
After discretization in space (and time):

$$\begin{aligned} g(x_{k+1}, x_k, u_k, \theta) &= 0 & \dim(x) \approx 10^4 - 10^6 \\ y_k &= h(x_k) \end{aligned}$$

and θ typically the permeabilities in each grid block

Properties of a Reservoir Model

- Coupled pde's
- Large number of states:
 - built up out of grid blocks
 - $10^2 - 10^6$ states variables
- Long simulation times
 - Up to several hours, even days
- Highly non-linear
 - Mainly due to different fluid properties of oil & water
- MIMO
 - $10^1 - 10^2$ injection & production wells



Model-based Life-Cycle Optimization

Net present value (NPV):

- Goal: optimize economic cost function related to oil recovery, as a function of dynamic **valve settings** (injection and production wells)

$$J = \sum_{k=1}^N \frac{\Delta(t_k)[r_o q_{o,k} - r_w q_{w,k} - r_i q_{i,k}]}{(1 + b)^{\frac{t_k}{\tau}}}$$

Under constraints: $c(x_k, u_k) \leq 0$

typically limits on water injection capacity, and max/min pressures in injection/production wells

Model-based Life-Cycle Optimization

Optimization problem:

$$\max_q J(q) = \max_q \sum_{k=1}^N L(x_k, q_k)$$

such that: $g(x_{k+1}, x_k, q_{i,k}) = 0, \quad x_0 = x(0)$

$$q_{min} \leq q_k \leq q_{max}$$

$$q_{o,k} + q_{w,k} = q_{i,k}$$

Non-convex optimization, solved by gradient-based method:
Adjoint-variables calculation through backward integration of
the related (Hamiltonian based adjoint) equation.

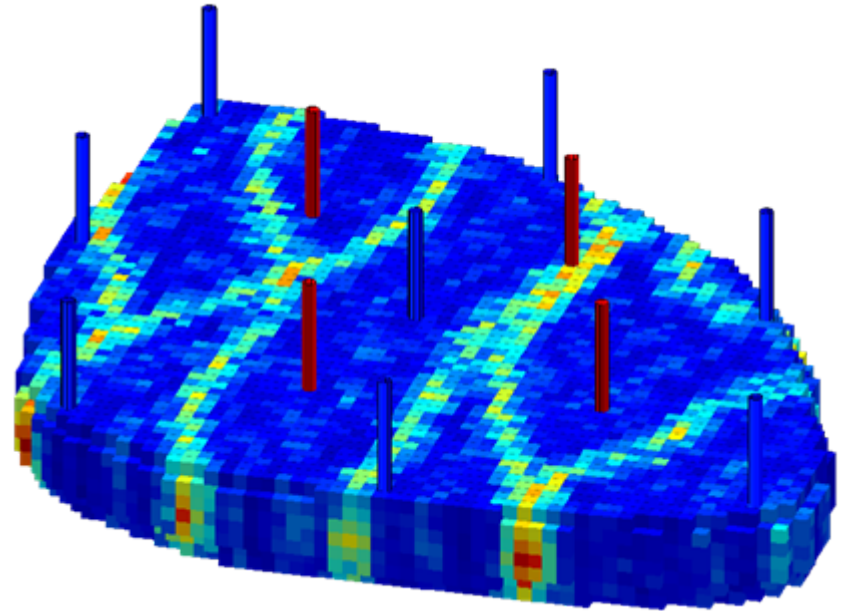
(feasible for systems of this size)

Contents

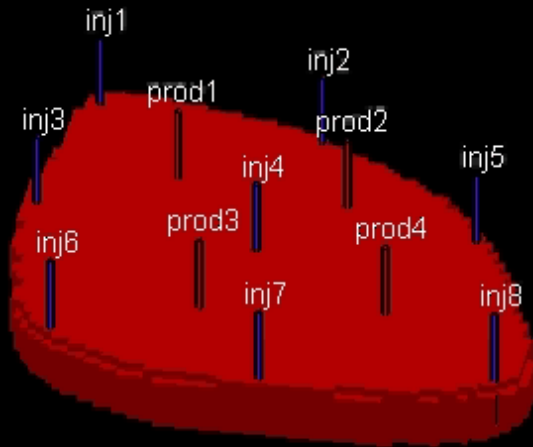
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12-well example

- 3D reservoir
- 8 injection / 4 production wells
- Period of 10 years
- High-permeability channels
- 18.553 grid blocks
- Minimum rate of 0.1 *stb/d*
- Maximum rate of 400 *stb/d*
- No discount factor
- $r_o = 20$ *\$/stb*, $r_w = 3$ *\$/stb* and $r_i = 1$ *\$/stb*
- **Optimization of economic benefit**



(Gijs van Essen et al.,
CAA 2006)



Reactive Control

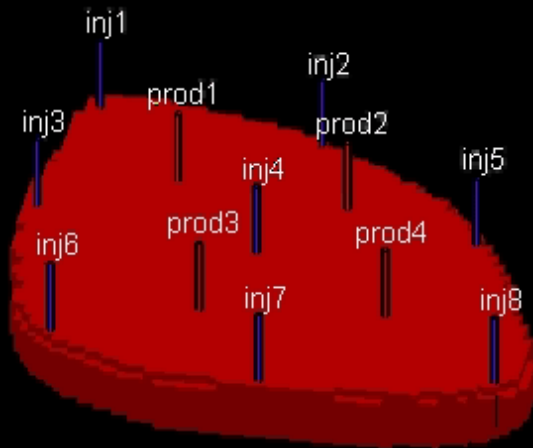
inj1
inj2
inj3
inj4
inj5
inj6
inj7
inj8
prod1
prod2
prod3
prod4

flow-rate

Cumulative Data

Oil Production: 0.00×10^6 bbl
Water Production: 0.00×10^6 bbl
Water Injection: 0.00×10^6 bbl

Revenue: 0.0 M\$



Optimal Control

inj1
inj2
inj3
inj4
inj5
inj6
inj7
inj8
prod1
prod2
prod3
prod4

flow-rate

Cumulative Data

Oil Production: 0.00×10^6 bbl
Water Production: 0.00×10^6 bbl
Water Injection: 0.00×10^6 bbl

Revenue: 0.0 M\$

time = 0.00 year

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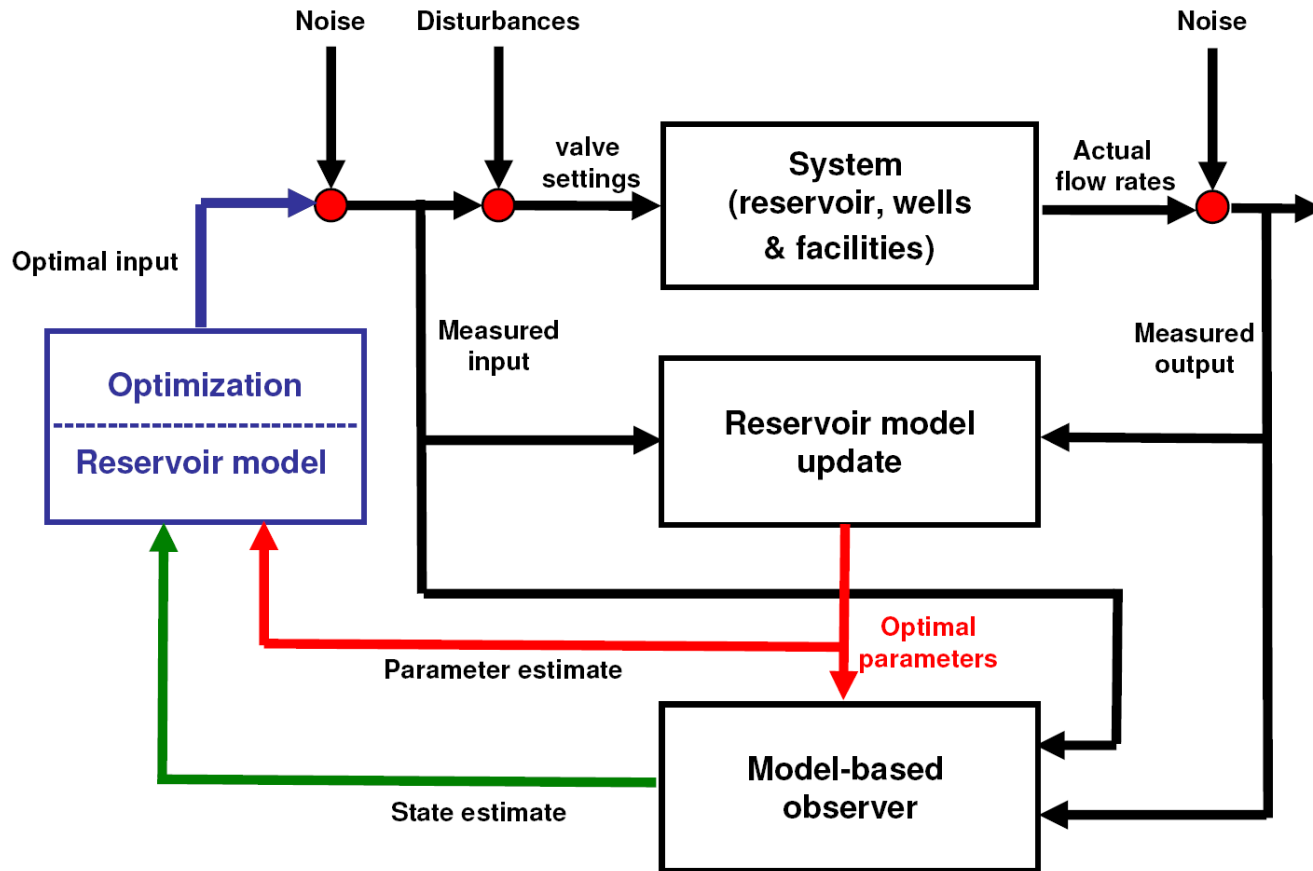
Closed-loop Reservoir Management

- Moving from (batch-wise) open-loop optimization to on-line closed-loop control
- However we need a model as a basis for e.g. a receding/shrinking horizon strategy

Obtaining a model

- First-principle models (geology) are very much uncertain
- Opportunities for identification are limited (nonlinear behaviour dependent on front-location, single batch process, experimental limitations)
- Option: estimate physical parameters (permeabilities) in first principles model; starting with initial guess

Closed-loop Reservoir Management



Closed-loop Reservoir Management

Receding/shrinking horizon control strategy:

- Use a state-estimator to reconstruct the current state
- Run the optimization algorithm to evaluate future scenario's
- Implement the optimized valve settings until the next state update
- This is actually a NMPC in a shrinking horizon implementation
- However no trajectory following but trajectory finding, i.e. real-time dynamic optimization (RTO)

Closed-loop Reservoir Management

Several options for nonlinear state and parameter estimation:

Available from oceanographic domain:

Ensemble Kalman filter (EnKF) (Evensen, 2006)

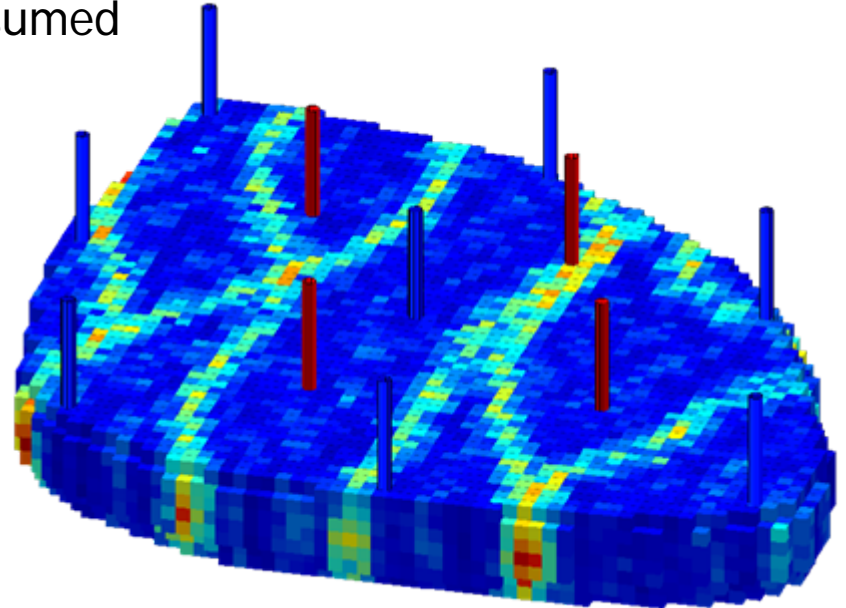
- Kalman type estimator, with analytical error propagation replaced by Monte Carlo approach (error cov. matrix determined by processing ensemble of model realizations)
- Ability to handle model uncertainty (in some sense)
- In reservoir engineering used for estimation of states **and parameters** (history matching)

Ensemble Kalman Filter

- As prior information an ensemble of initial states $\{\hat{x}_{k|k}\}$ is generated from a given distribution
- By simulating every ensemble member, corresponding ensembles $\{\hat{x}_{k+1|k}\}$ and $\{\hat{y}_{k+1|k}\}$ are generated, and stored as columns of matrices \hat{X} and \hat{Y} respectively
- The measurement update of a EKF is applied to every element of the ensemble, where the covariance matrices are replaced by sampled estimates on the basis of \hat{X} and \hat{Y} .
- The update becomes: $\hat{x}_{k+1|k+1} = \hat{x}_{k+1|k} + K_{k+1}[y_{k+1} - \hat{y}_{k+1|k}]$, where K_{k+1} is given by:
$$K_{k+1} = \hat{X}\hat{Y}^T \cdot [\hat{Y}\hat{Y}^T + R]^{-1} \quad (\text{BLUE})$$
- The result is a new ensemble $\{\hat{x}_{k+1|k+1}\}$

Closed-loop simulation example

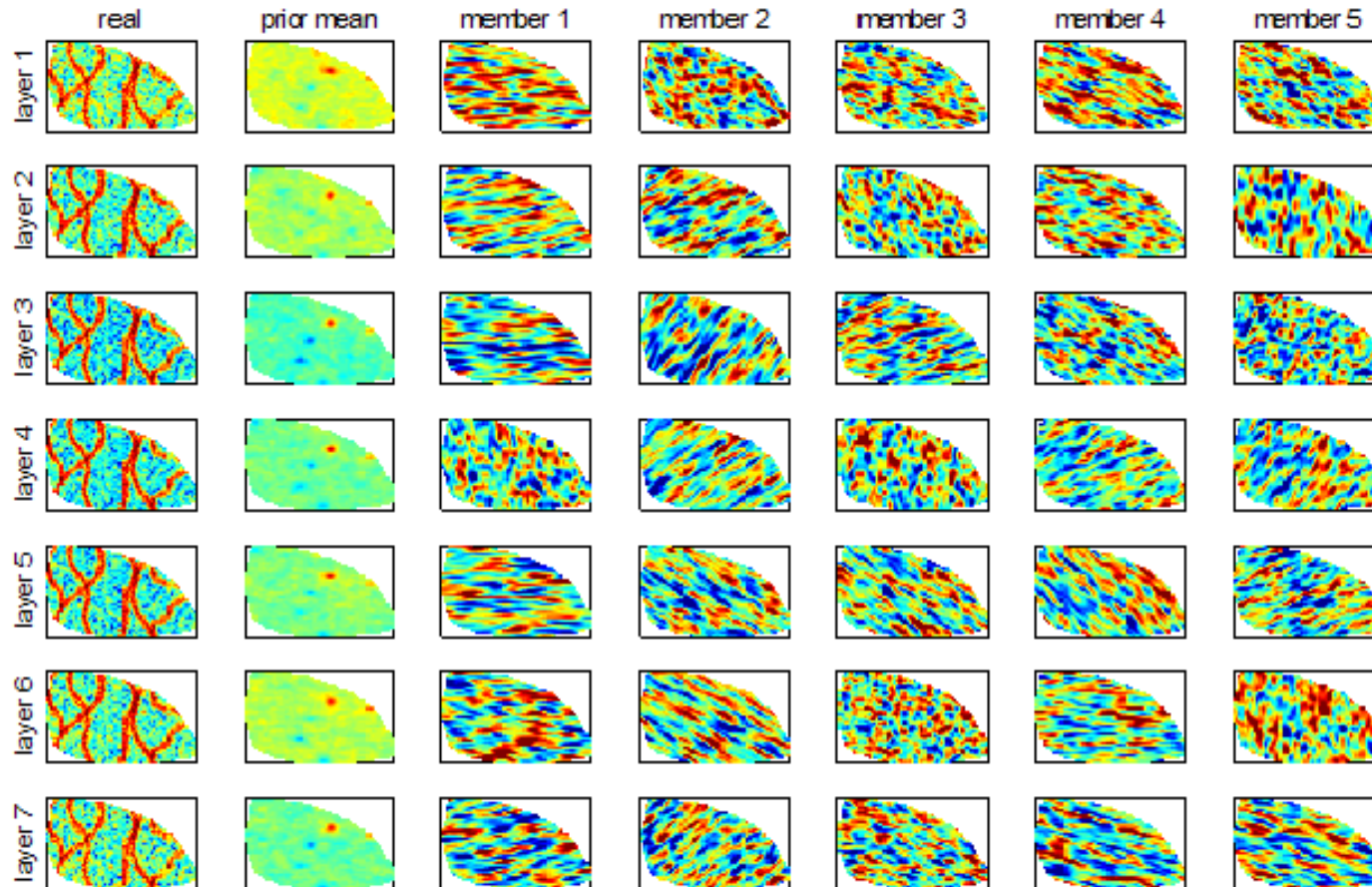
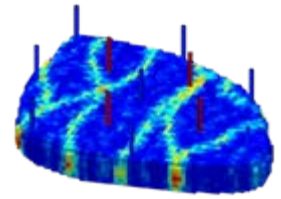
- Model with high-perm channels assumed to be 'reality'
- Permeabilities are unknown in closed-loop control
- Period of **8 years**
- Objective function: **NPV**
 - $r_o = 10$ \$/stb, $r_w = 1$ \$/stb and $r_i = 0$ \$/stb
 - Annual discount factor: **15%**
- Measurements
 - Fractional flow rates (oil/water)
 - Bottom-hole pressures
- Yearly updates of parameters and control strategy



Gijs van Essen, 2006

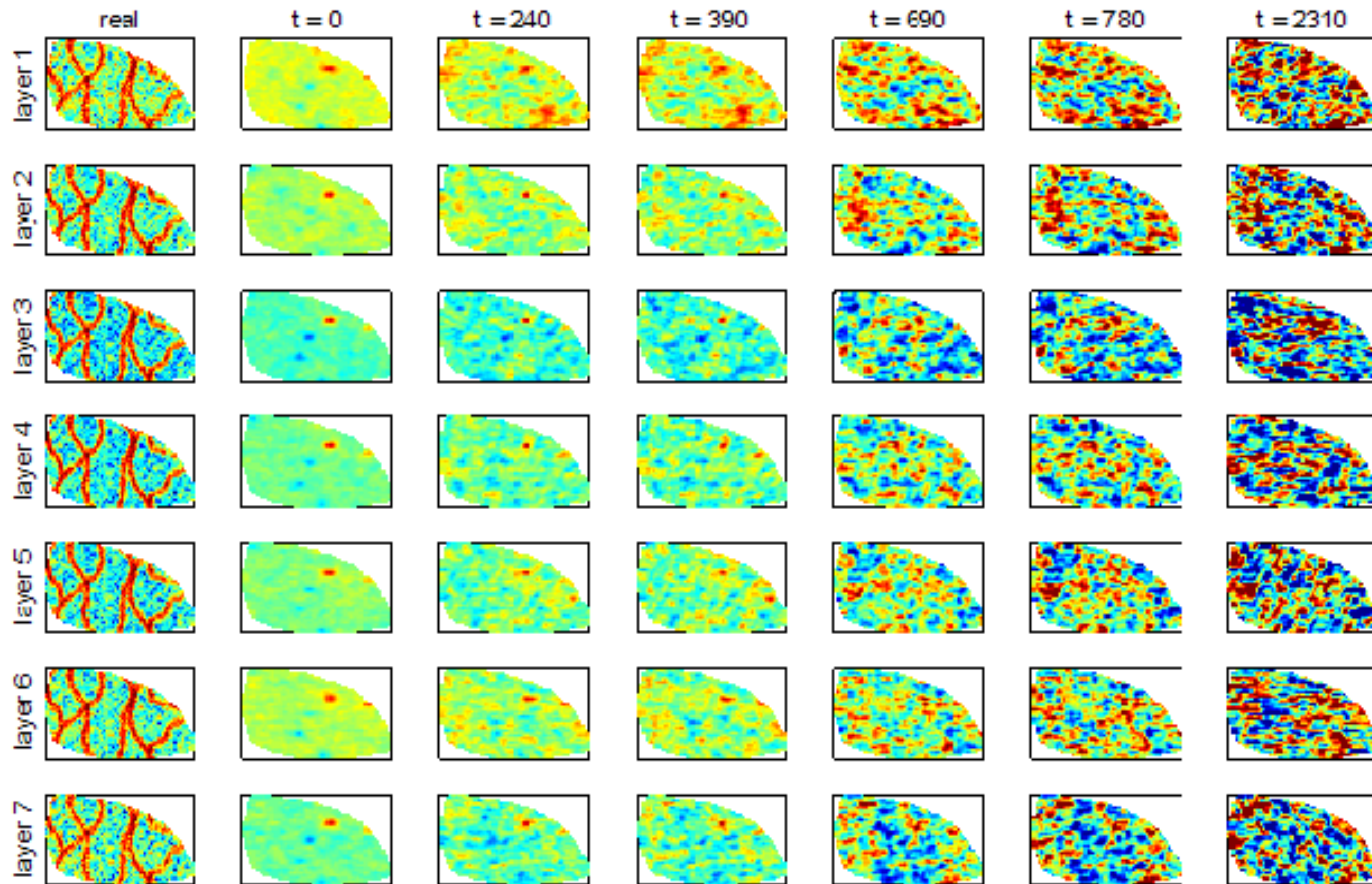
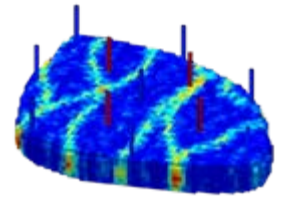
Closed-loop simulation example

Initial ensemble



Closed-loop simulation example

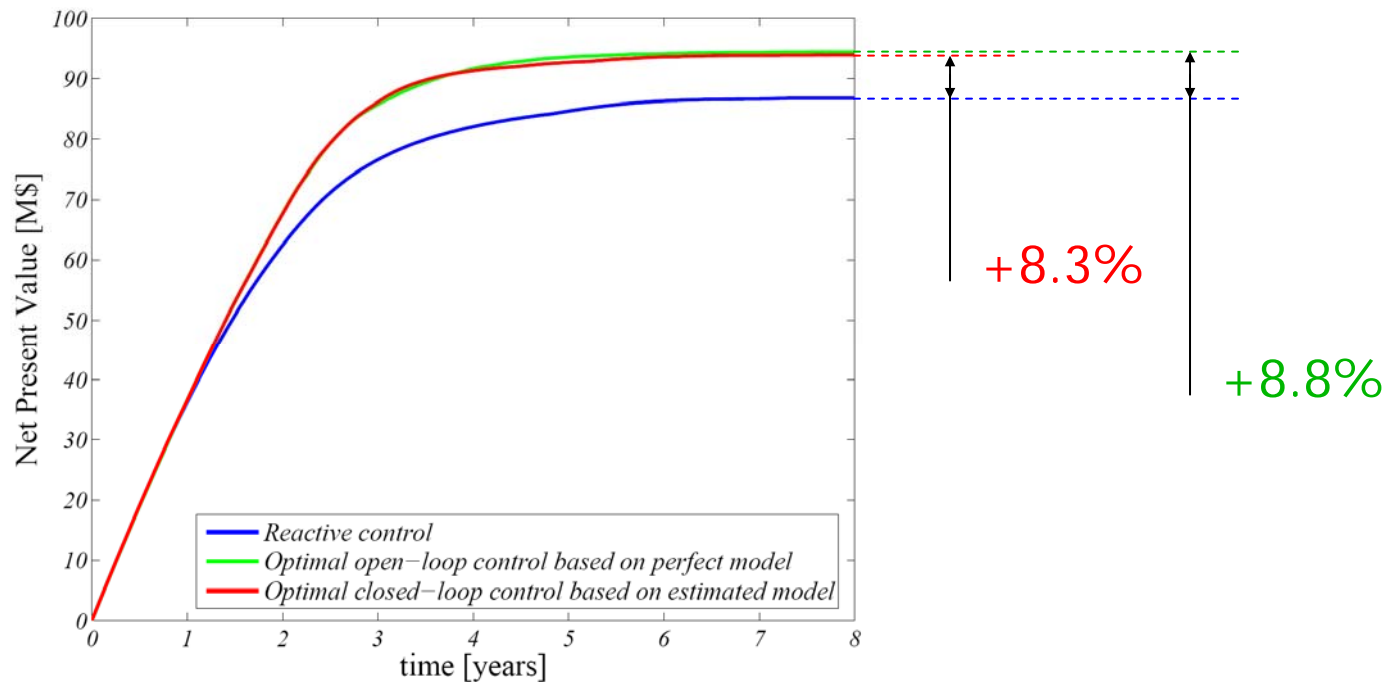
Ensemble updates at different times



Closed-loop simulation example

Results

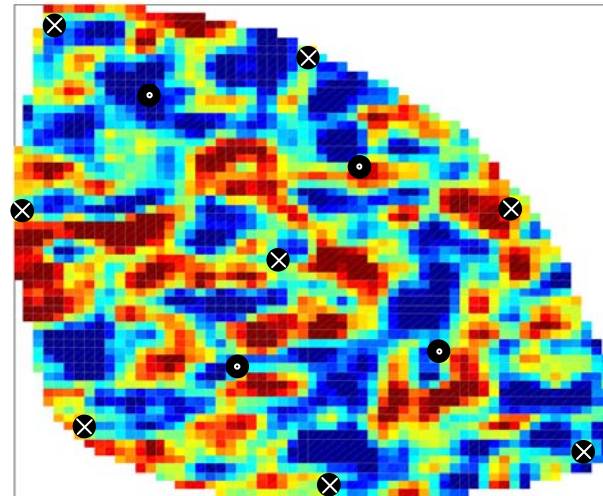
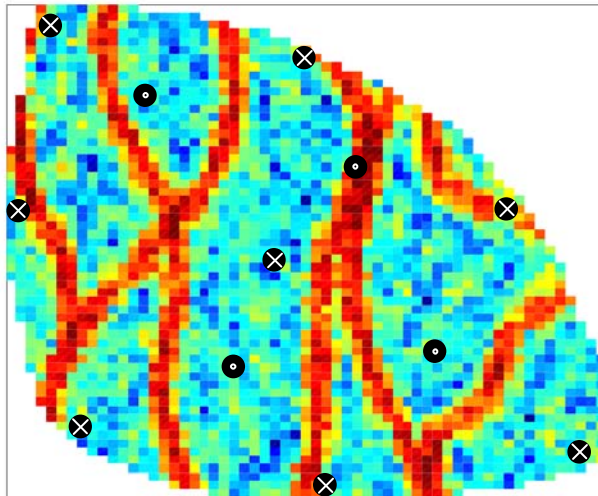
- 3 study cases: reactive control, optimal open-loop control based on perfect ('reality') model, optimal closed-loop control



Closed-loop reservoir management

Questions:

- Why are such poor models working so well?
- Does this mean that we don't need geology?



Reservoir dynamics live in low-order space

- **Observation and control in the wells**
 - Models will typically be poorly observable and/or poorly controllable
 - Real (local) input-output dynamics is of limited order
- **Parameter estimation:**
 - Physical parameters (permeabilities) determine predictive quality but one parameter per grid block leads to excessive over-parametrization (not to be validated)

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Parameter estimation and identifiability

- Through one parameter per grid block: close connection between states and parameters
- When estimating parameters (as states) in EnKF:
 - Data not sufficiently informative to estimate all parameters
 - Parameters are updated only in directions where data contains information

Result and reliability is crucially dependent on initial state/model

Parameter estimation and identifiability

- Lack of identifiability: different parameters lead to same cost function
- In sequential (Bayesian) approach to state/parameter estimation lack of identifiability is hardly observed:
- Cost function:

$$V_p(\theta) = V(\theta) + \frac{1}{2}(\theta - \theta_p)^T P_p^{-1}(\theta - \theta_p)$$

$$V(\theta) := \frac{1}{2}\epsilon(\theta)^T P_v^{-1}\epsilon(\theta), \quad \epsilon(\theta) = \mathbf{y} - \hat{\mathbf{y}}(\theta)$$

- Analysis of $V(\theta)$ can show identifiable directions (locally)

Parameter estimation and identifiability

Option:

Calculate the identifiable subspace of the parameter domain

At a particular point $\hat{\theta}$ the identifiable subspace of Θ can be computed! This leads to a map

$$\rho = T\theta \quad \text{with} \quad \dim(\rho) \ll \dim(\theta)$$

See Van Doren et al. (IFAC 2008)

Tool: analyse (svd) the matrix $\frac{\partial^2 V(\theta)}{\partial \theta^2} = \frac{\partial \hat{y}(\theta)^T}{\partial \theta} P_v^{-1} \left(\frac{\partial \hat{y}(\theta)^T}{\partial \theta} \right)^T$,

$$\frac{\partial \hat{y}(\theta)^T}{\partial \theta} P_v^{-\frac{1}{2}} = \begin{bmatrix} U_1 & U_2 \end{bmatrix} \begin{bmatrix} \Sigma_1 & 0 \\ 0 & \Sigma_2 \end{bmatrix} \begin{bmatrix} V_1^T \\ V_2^T \end{bmatrix} \longrightarrow \rho = U_1^T \theta$$

Limitation: only local linearized situation can be handled

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Additional optimization opportunities

- Well location optimization
- Well design & trajectory optimization
- Robust Optimization
- Multi-objective/hierarchical optimization
(balancing long-term and short-term objectives/actions)

Discussion

- Challenging problems in model-based operation on the basis of highly uncertain information
- Key elements:
 - **Model-based optimization** under physical constraints and geological **uncertainties**
 - Appropriate merging of **physical and measured data** in **low-order** reliable and **goal-oriented models**
 - Challenging **parametrization** issues, in relation to controllability, observability and **identifiability**
 - **Learning** the optimal strategy in one shot (batch)

J.D. Jansen, O.H. Bosgra and P.M.J. Van den Hof, Model-based control of multiphase flow in subsurface oil reservoirs, *Journal of Process Control*, 18, 846-855, 2008.

Questions?

