



Single module identification - full MISO with direct and indirect method

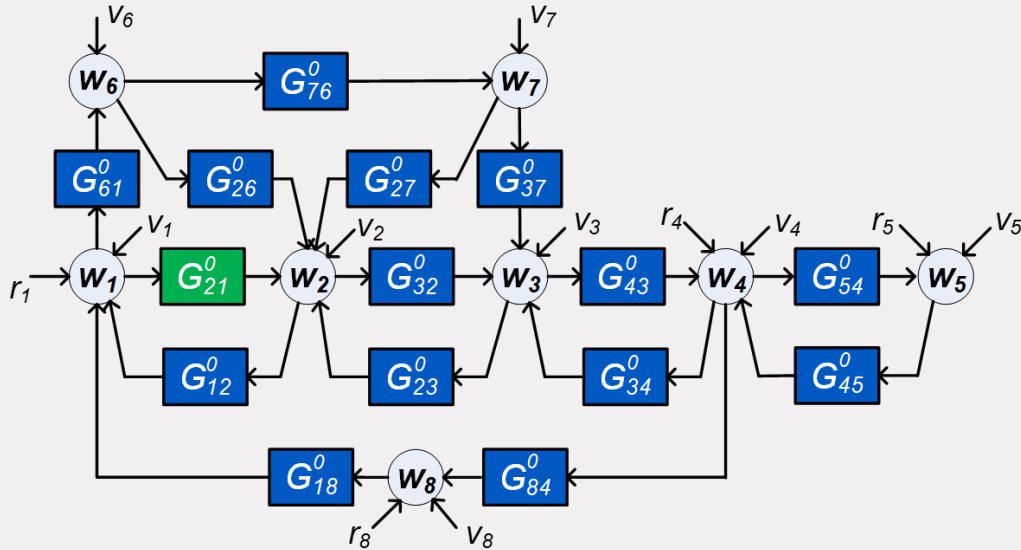
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Single module identification



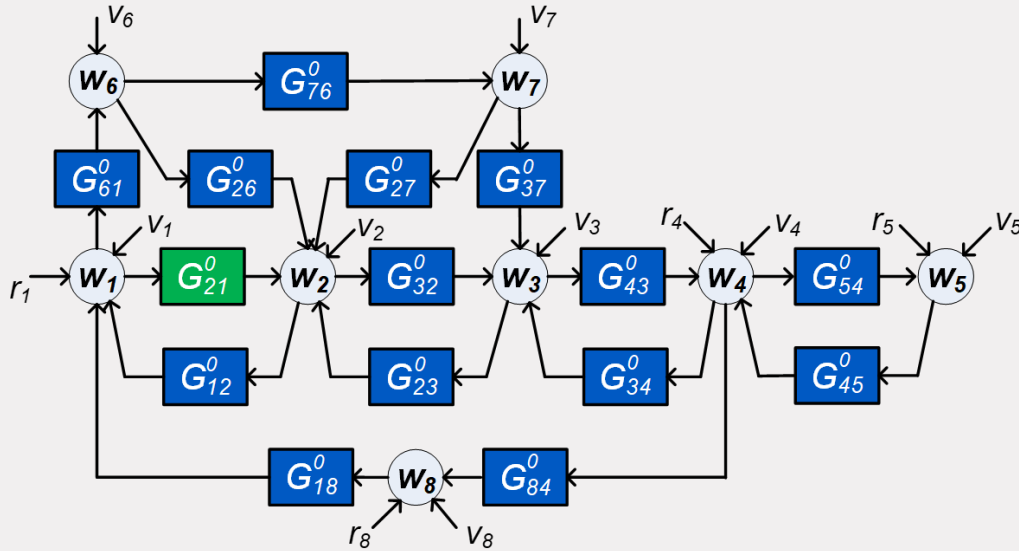
The problem:

For a network with known topology:

Identify G_{21}^0 on the basis of selected measured signals (w, r)

Preference for “local” measurements and limited excitation

Single module identification



Option:

Identify the full MIMO network:

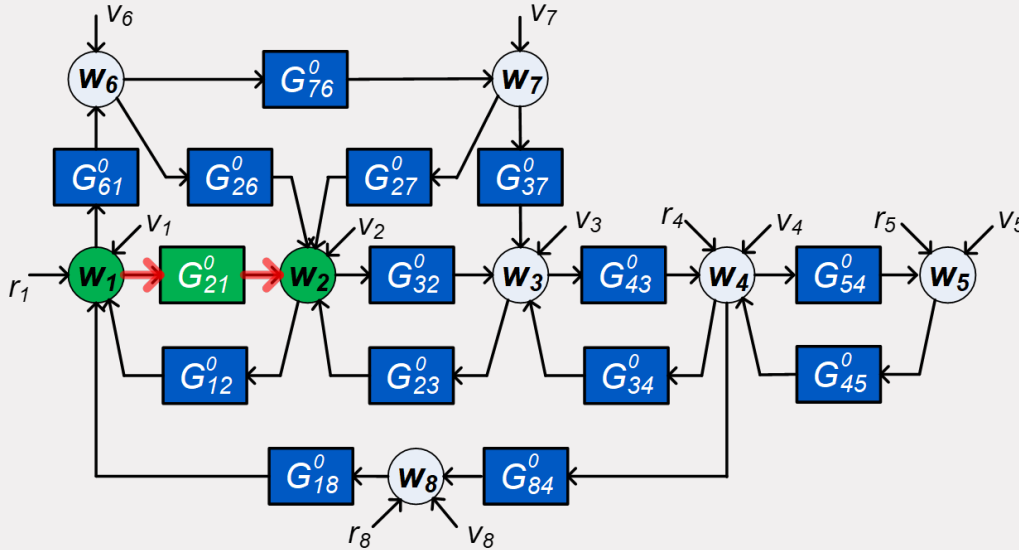
$$\begin{aligned} w &= (I - G^0)^{-1} [R^0 r + H^0 v] \\ &= T_{wr} r + T_{we} e \end{aligned}$$

and recover \hat{G}_{21}^0 from the estimated model.

Consequence:

- Computational complexity
- High demand on excitation and sensing of signals

Single module identification



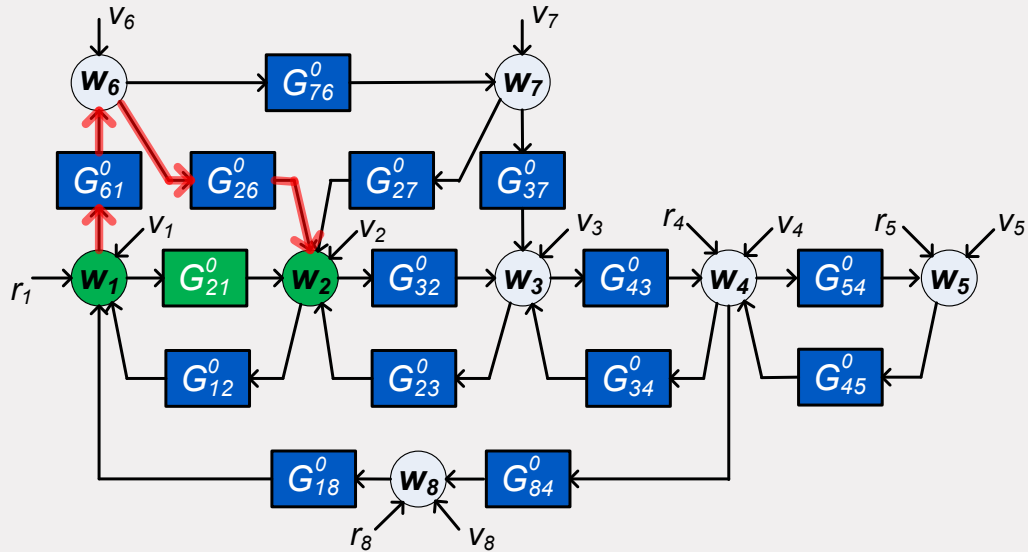
Naïve local approaches:

- identify based on w_2 and w_1 ; or
- identify based on $T_{w_2 r_1} T_{w_1 r_1}^{-1}$

do not work,

e.g. because of parallel paths

Single module identification



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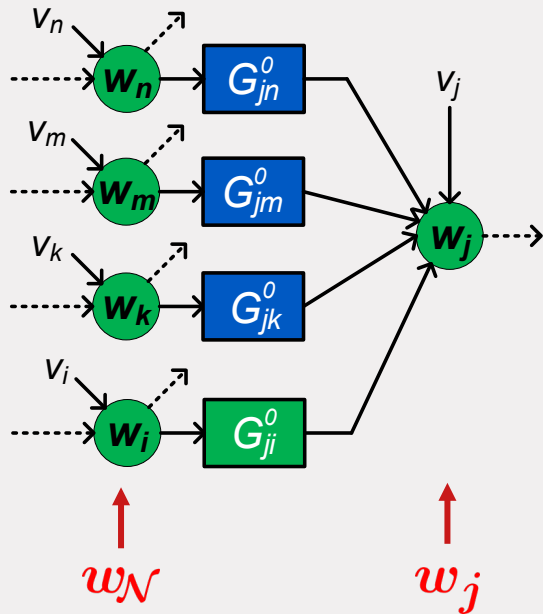
e.g. because of parallel paths

The “observed” transfer function between w_1 and w_2 is not necessarily G_{21}^0 .

Single module identification – Full MISO situation

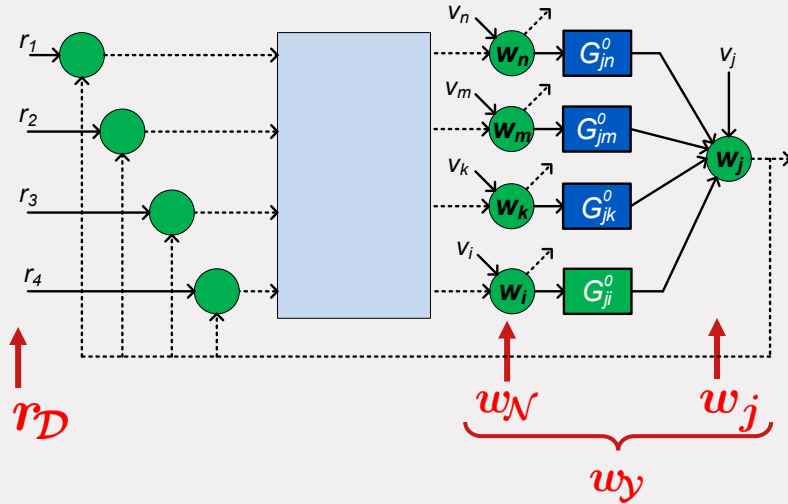
Full MISO situation:

Measure output $w_j = w_2$ of target module and all in-neighbors $w_{\mathcal{N}}$ of w_j



Multi-input single-output identification problem
to be addressed by a closed-loop identification
method
(direct or indirect method)

Indirect methods



MISO identification problem

- Select output w_j and all its in-neighbors w_N as predictor output; r_D as predictor input
- Estimate \bar{T}_{Nr} and \bar{T}_{jr} consistently, and determine:

$$\hat{G}_{jN} = \hat{T}_{jr} \hat{T}_{Nr}^{-1} \quad [1]$$
- or through IV or two-stage method^[2]
- freedom in location of r-signals (e.g. directly on w_N)

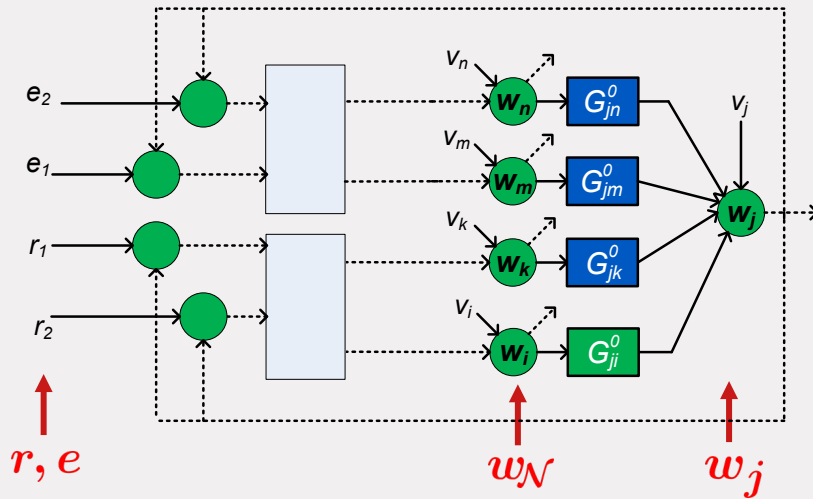
Condition for consistency of \hat{G}_{ji} :

- $G^0 \in \mathcal{G}$, no noise model required
- r_D persistently exciting, $\Phi_{r_D}(\omega) > 0$, at a sufficient number of ω
- Typically, $\dim(r_D) \geq \dim(w_N)$

[1] Gevers et al., SYSID 2018; Hendrickx et al, TAC 2019; Bazanella et al., CDC 2019

[2] VdHof et al., Automatica 2013; Dankers et al., Automatica 2015

Direct method



- + Excitation through both r and e signals
- + Consistency + minimum variance (ML)

$$\varepsilon(t, \theta) = \bar{H}(q, \theta)^{-1} [w_y(t) - \bar{G}(q, \theta)w_N(t)]$$

- Estimate transfer $w_N \rightarrow w_j$ and model the disturbance process on the output.
- provided there is enough excitation, through external signals r and e

Conditions for consistency of \hat{G}_{ji} :

- $S \in \mathcal{M}$
- $\Phi_v(\omega)$ is diagonal
- Every loop around w_j has a delay
- $\Phi_\kappa(\omega) > 0$ with $\kappa(t) = \begin{bmatrix} w_j(t) \\ w_N(t) \end{bmatrix}$ ⁽¹⁾

[1] VdHof et al., Automatica 2013;
 [2] VdHof and Ramaswamy, CDC 2020;
 [3] Bombois et al., Automatica, 2023

Summary full MISO case – direct and indirect method

- All local nodes are measured To be relaxed later on
- Closed-loop identification concepts (direct / indirect) can be used

Indirect method:

- No noise models required
- More “expensive” experiments

Direct method:

- Noise models required
- Minimum variance results
- Requires a diagonal noise spectrum To be relaxed later on

Both methods: non-convex algorithms are poorly scalable to large dimensions